

## Bäcklund transformations of $n$ -dimensional constant torsion curves

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**Abstract.** The Bäcklund transformation of two surfaces of  $\mathbf{R}^3$  with the same constant negative Gaussian curvature transforms an asymptotic line of one surface into an asymptotic line of the other. Since by Enneper the asymptotic lines of such a surface have constant torsion, it is natural to restrict the Bäcklund transformations to such curves. This idea was developed by ANNALISA CALINI and THOMAS IVEY in [2]. We shall prove the converse of their theorem and generalize the transformation for the  $n$ -dimensional case.

### 0. Introduction

By the work of Bianchi and Lie it is possible to compute the Gaussian curvature of the focal surfaces of a line congruence in terms of the coefficients of the first fundamental form for the spherical representation and the distance between the corresponding limit points of these surfaces (see [3]).

Bäcklund proved that for pseudospherical congruences satisfying the two additional conditions that the distance  $r$  between corresponding limit points is constant and that the normals of the focal surfaces at these points form a constant angle  $\theta$ , the curvatures must be equal to the same negative constant  $-\sin^2 \theta / r^2$  (see [3]). By Enneper's relation between the first, second and third fundamental forms of a surface of negative Gaussian curvature the relation  $\tau^2 = -K$  between the torsion  $\tau$  of an asymptotic line

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and the curvature  $K$  holds. When the curvature is constant the torsion cannot change. Bearing in mind that under pseudospherical congruences asymptotic lines correspond, these provide a method for restricting the Bäcklund transformation to constant torsion curves. This was done by ANNALISA CALINI and THOMAS IVEY in [2]. They constructed a constant torsion curve from a given one. We prove the converse of their theorem, namely: If there is a correspondence  $\nu$  between the points of two unit speed curves  $\mathbf{c}, \tilde{\mathbf{c}}$  having the property that the line joining the corresponding points  $\mathbf{c}(s)$  and  $\tilde{\mathbf{c}}(s) = \nu(\mathbf{c}(s))$  is the intersection of the osculating planes of these curves, and this intersection has the same angle with the curves, the line segment  $\mathbf{c}(s)\tilde{\mathbf{c}}(s)$  has constant length  $r$  and the binormals in corresponding points form a constant angle  $\theta$ , then the curves have the same constant torsion  $\sin \theta/r$ .

We could not find a connection between the sectional curvature of an  $n$ -dimensional manifold of constant negative curvature in the  $2n - 1$ -dimensional euclidean space and the curvatures of its asymptotic lines in order to restrict the generalized Bäcklund transformation (see [4], and [5]) to curves in  $2n - 1$ -dimensional euclidean spaces.

However if we consider just the transformation of Annalisa Calini and Thomas Ivey [2] for 3-dimensional constant torsion curves we can generalize it for higher dimensions.

### 1. Bäcklund transformations of 3-dimensional constant torsion curves

In [3] A. Calini and T. Ivey constructed a curve of constant torsion from a given one. We shall prove that under some assumptions made for a transformation between two curves they must have the same constant torsion.

**Theorem 1.1.** *Suppose that  $\nu$  is a transformation between two curves  $\mathbf{c}$  and  $\tilde{\mathbf{c}}$  of  $\mathbf{R}^3$  with  $\tilde{\mathbf{c}}(s) = \nu(\mathbf{c}(s))$ , where  $s$  is the arc length of  $\mathbf{c}$ , such that in corresponding points we have:*

- (1) *The line joining these points is the intersection of the osculating planes of the curves, such that the line segment  $\mathbf{c}(s)\tilde{\mathbf{c}}(s)$  has constant length  $r$ .*
- (2) *The vector  $\tilde{\mathbf{c}}(s) - \mathbf{c}(s)$  forms the same angle  $\beta \neq \pi/2$  with the tangent vectors of the curves.*

- (3) *The binormals of the curves form the same constant angle  $\theta \neq 0$ .  
Then the torsions of the curves are equal to the same constant  $\sin \theta/r$ .*

PROOF. Denote by  $(\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3)$  the Frenet frame of  $\mathbf{c}$  and by  $(\tilde{\mathbf{e}}_1, \tilde{\mathbf{e}}_2, \tilde{\mathbf{e}}_3)$  that of  $\tilde{\mathbf{c}}$  in the corresponding points  $\mathbf{c}(s)$  and  $\tilde{\mathbf{c}}(s)$ . If we denote by  $\mathbf{f}_1$  the unit vector of  $\tilde{\mathbf{c}}(s) - \mathbf{c}(s)$ , then we can complete  $\mathbf{f}_1, \mathbf{e}_3$  and  $\mathbf{f}_1, \tilde{\mathbf{e}}_3$  to the positively oriented orthonormal frames  $(\mathbf{f}_1, \mathbf{f}_2, \mathbf{e}_3)$  and  $(\mathbf{f}_1, \tilde{\mathbf{f}}_2, \tilde{\mathbf{e}}_3)$  respectively. Let  $\mathbf{f}_3 = \mathbf{e}_3, \tilde{\mathbf{f}}_3 = \tilde{\mathbf{e}}_3$  and  $-\beta$  be the angle between  $\mathbf{f}_1$  and  $\mathbf{e}_1$ . Then the angle between  $\mathbf{f}_1$  and  $\tilde{\mathbf{e}}_1$  is also  $-\beta$ . Thus we can obtain the frames  $(\mathbf{f}_1, \mathbf{f}_2, \mathbf{f}_3)$  and  $(\mathbf{f}_1, \tilde{\mathbf{f}}_2, \tilde{\mathbf{f}}_3)$  by rotating the frames  $(\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3)$  and  $(\tilde{\mathbf{e}}_1, \tilde{\mathbf{e}}_2, \tilde{\mathbf{e}}_3)$  around  $\mathbf{e}_3$  and  $\tilde{\mathbf{e}}_3$  respectively with angle  $-\beta$ . Analytically this can be written as:

$$(1.1) \quad \begin{cases} \mathbf{f}_1 = \cos \beta \mathbf{e}_1 + \sin \beta \mathbf{e}_2, \\ \mathbf{f}_2 = -\sin \beta \mathbf{e}_1 + \cos \beta \mathbf{e}_2, \\ \mathbf{f}_3 = \mathbf{e}_3, \end{cases}$$

and

$$(1.2) \quad \begin{cases} \mathbf{f}_1 = \cos \beta \tilde{\mathbf{e}}_1 + \sin \beta \tilde{\mathbf{e}}_2, \\ \tilde{\mathbf{f}}_2 = -\sin \beta \tilde{\mathbf{e}}_1 + \cos \beta \tilde{\mathbf{e}}_2, \\ \tilde{\mathbf{f}}_3 = \tilde{\mathbf{e}}_3. \end{cases}$$

Since  $\mathbf{f}_3 = \mathbf{e}_3, \tilde{\mathbf{f}}_3 = \tilde{\mathbf{e}}_3$  and the angle between  $\mathbf{e}_3, \tilde{\mathbf{e}}_3$  is the constant  $\theta$ , we can obtain the frame  $(\mathbf{f}_1, \tilde{\mathbf{f}}_2, \tilde{\mathbf{f}}_3)$  by rotating the frame  $(\mathbf{f}_1, \mathbf{f}_2, \mathbf{f}_3)$  around  $\mathbf{f}_1$  with angle  $\theta$ . Thus we have:

$$(1.3) \quad \begin{cases} \tilde{\mathbf{f}}_2 = \cos \theta \mathbf{f}_2 - \sin \theta \mathbf{f}_3, \\ \tilde{\mathbf{f}}_3 = \sin \theta \mathbf{f}_2 + \cos \theta \mathbf{f}_3. \end{cases}$$

Using (1.1), (1.2) and (1.3) we can express  $\tilde{\mathbf{e}}_1, \tilde{\mathbf{e}}_2, \tilde{\mathbf{e}}_3$  in terms of  $\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3$  as follows:

$$(1.4) \quad \begin{cases} \tilde{\mathbf{e}}_1 = \mathbf{e}_1 + (1 - \cos \theta) \sin \beta (\cos \beta \mathbf{e}_2 - \sin \beta \mathbf{e}_1) + \sin \theta \sin \beta \mathbf{e}_3, \\ \tilde{\mathbf{e}}_2 = \mathbf{e}_2 - (1 - \cos \theta) \cos \beta (\cos \beta \mathbf{e}_2 - \sin \beta \mathbf{e}_1) - \sin \theta \cos \beta \mathbf{e}_3, \\ \tilde{\mathbf{e}}_3 = \cos \theta \mathbf{e}_3 + \sin \theta (\cos \beta \mathbf{e}_2 - \sin \beta \mathbf{e}_1). \end{cases}$$

Bearing in mind that the distance between  $\mathbf{c}(s)$  and  $\tilde{\mathbf{c}}(s)$  is the constant  $r$  and  $\mathbf{f}_1 = \cos \beta \mathbf{e}_1 + \sin \beta \mathbf{e}_2$ , we have:

$$(1.5) \quad \tilde{\mathbf{c}}(s) = \mathbf{c}(s) + r(\cos \beta \mathbf{e}_1 + \sin \beta \mathbf{e}_2).$$

Differentiating  $(\tilde{\mathbf{c}} - \mathbf{c})^2 = r^2$  we obtain  $2(\tilde{\mathbf{c}} - \mathbf{c})(\dot{\tilde{\mathbf{c}}}|\tilde{\mathbf{e}}_1 - \mathbf{e}_1) = 0$ . Since  $\tilde{\mathbf{c}} - \mathbf{c} = r\mathbf{f}_1$ , this yields  $|\dot{\tilde{\mathbf{c}}}| \cos \beta - \cos \beta = 0$ , so that  $\tilde{\mathbf{c}}$  is also of unit speed.

Using the Frenet formulae for  $\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3$  it is easy to see that  $\tilde{\mathbf{e}}_1, \tilde{\mathbf{e}}_2, \tilde{\mathbf{e}}_3$  given by (1.4) satisfy the Frenet formulae if and only if:  $\tilde{K}_1 = K_1 - 2C \sin \beta$ ,  $\tilde{K}_2 = K_2$  and  $d\beta/ds = C \sin \beta - K_1$ , where  $K_1, \tilde{K}_1$  and  $K_2, \tilde{K}_2$  are the curvatures and torsions of  $\mathbf{c}$  and  $\tilde{\mathbf{c}}$  respectively, and  $C = K_2 \tan \theta/2$ .

By (1.5) we have:

$$\tilde{\mathbf{e}}_1 = \left(1 - rK_2 \tan \frac{\theta}{2} \sin^2 \beta\right) \mathbf{e}_1 + rK_2 \tan \frac{\theta}{2} \sin \beta \cos \beta \mathbf{e}_2 + rK_2 \sin \beta \mathbf{e}_3.$$

Comparing this with (1.4)<sub>1</sub> we obtain  $K_2 = \sin \theta/r$ . Thus the the curves  $\mathbf{c}$  and  $\tilde{\mathbf{c}}$  have the same constant torsion

$$\tilde{K}_2 = K_2 = \frac{\sin \theta}{r},$$

and the transformation can be given by

$$\tilde{\mathbf{c}} = \mathbf{c} + \frac{2C}{C^2 + K_2^2} (\cos \beta \mathbf{e}_1 + \sin \beta \mathbf{e}_2),$$

where

$$\frac{d\beta}{ds} = C \sin \beta - K_1.$$

The last two equations are the defining relations of the transformation given by A. CALINI and T. IVEY in Theorem 1.1 of [3]. Examples for such transformation are given in [3].

## 2. Bäcklund transformations of $n$ -dimensional constant torsion curves

From now on we mean by the torsion of a curve its last curvature. Let  $\mathbf{c}$  and  $\tilde{\mathbf{c}}$  be two curves in  $\mathbf{R}^n$ , with curvatures  $K_1, \dots, K_{n-1}$  and  $\tilde{K}_1, \dots, \tilde{K}_{n-1}$  respectively. Then the main theorem of Section 1 can be generalized as follows:

**Theorem 2.1.** *Suppose that  $\nu$  is a transformation between  $\mathbf{c}$  and  $\tilde{\mathbf{c}}$  with  $\tilde{\mathbf{c}}(s) = \nu(\mathbf{c}(s))$ , where  $s$  is the arclength of  $\mathbf{c}$  such that for correspond-*

ing points we have:

- (1) The line joining these points is contained in the intersection of the osculating hyperplanes and the line segment  $\mathbf{c}(s)\tilde{\mathbf{c}}(s)$  has constant length  $r$ .
- (2) (a) The angle between the vectors  $\mathbf{f}_1$  and  $\mathbf{e}_{n-1}$  is complementary to the angle between the vectors  $\mathbf{e}_1$  and  $\mathbf{f}_{n-1}$ , where  $\mathbf{f}_1$  is the unit vector of  $\tilde{\mathbf{c}}(s) - \mathbf{c}(s)$ ,  $(\mathbf{f}_1, \dots, \mathbf{f}_{n-2})$  and  $(\mathbf{f}_1, \dots, \mathbf{f}_{n-2}, \mathbf{f}_{n-1}, \mathbf{e}_n)$  are positively oriented frames of the intersection of the osculating planes and the whole space respectively and  $(\mathbf{e}_1, \dots, \mathbf{e}_n)$  is the Frenét frame of  $\mathbf{c}$ .  
 (b)  $\langle \mathbf{e}_1, \mathbf{f}_1 \rangle \neq 0$ , where  $\langle \cdot, \cdot \rangle$  is the standard scalar product of  $\mathbf{R}^n$ .
- (3) The Frenét frame of  $\tilde{\mathbf{c}}$  can be obtained from that of  $\mathbf{c}$  by a rotation with constant angle  $\theta \neq 0$  around a plane which contains  $\mathbf{e}_n$ .

Then the curves have the same constant torsion  $\sin \theta / r$ . Moreover for  $n \geq 4$  we have that

$$K_1 = \tilde{K}_1, \dots, K_{n-3} = \tilde{K}_{n-3}.$$

PROOF. From (3) we have  $\tilde{E} = A^T \Theta A E$ , where  $E^T = (\mathbf{e}_1, \dots, \mathbf{e}_n)$  and  $\tilde{E}^T = (\tilde{\mathbf{e}}_1, \dots, \tilde{\mathbf{e}}_n)$  are the Frenét frames of  $\mathbf{c}$  and  $\tilde{\mathbf{c}}$ ,

$$\Theta = \begin{vmatrix} I_{n-2} & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{vmatrix}$$

and  $A \in SO(n)$  such that  $a_{in} = a_{ni} = \delta_{in}$ , where  $\delta_{ij}$  is the Kronecker symbol. In terms of the entries this can be written as:

$$(2.1) \quad \begin{cases} \tilde{\mathbf{e}}_i = \sum_{j=1}^{n-1} [\delta_{ij} - a_{n-1,i} a_{n-1,j} (1 - \cos \theta)] \mathbf{e}_j - a_{n-1,i} \sin \theta \mathbf{e}_n; \\ i = \overline{1, n-1}, \\ \tilde{\mathbf{e}}_n = \sin \theta \sum_{j=1}^{n-1} a_{n-1,j} \mathbf{e}_j + \cos \theta \mathbf{e}_n. \end{cases}$$

Since the first  $n - 2$  columns and rows of  $\Theta$  form an identity matrix and  $a_{in} = a_{ni} = \delta_{in}$ ,  $A\tilde{E} = \Theta A E$  implies that the first  $n - 2$  rows of  $A E$  are equal to the first  $n - 2$  columns of  $A\tilde{E}$  and form the basis  $(\mathbf{f}_1, \dots, \mathbf{f}_{n-2})$  for the intersection of the osculating hyperplanes. Thus  $F^T = (\mathbf{f}_1, \dots, \mathbf{f}_{n-1}, \mathbf{e}_n)$ , where  $F = A E$ .

By (2)(a) we also have

$$(0) \quad a_{1,n-1} = -a_{n-1,1},$$

where  $A = (a_{ij})_{1 \leq i, j \leq n}$ . Differentiating (2.1) and using the Frenét formulae for  $E$ ,  $\tilde{E} = (\tilde{\mathbf{e}}_1, \dots, \tilde{\mathbf{e}}_n)$  satisfies the Frenét formulae of  $\tilde{\mathbf{c}}$  if and only if the following groups of relations hold:

$$(I) \quad a_{n-1,2} = a_{n-1,n-1} = 0, \quad \text{if } n \geq 4,$$

$$\tilde{K}_{n-2} = K_{n-2} + 2K_{n-1} \tan \frac{\theta}{2} a_{n-1,n-2},$$

$$(II) \quad \begin{cases} a_{n-1,1} = -K_1 a_{n-1,2} + K_{n-1} a_{n-1,n-1} a_{n-1,1} \tan \frac{\theta}{2}, \\ a_{n-1,j} = K_j a_{n-1,j+1} - K_{j-1} a_{n-1,j-1} \\ \quad + K_{n-1} a_{n-1,n-1} a_{n-1,j} \tan \frac{\theta}{2}; \quad j = \overline{2, n-2}, \\ a_{n-1,n-1} = -K_{n-2} a_{n-1,n-2} - K_{n-1} \tan \frac{\theta}{2} (1 - a_{n-1,n-1}^2), \end{cases}$$

$$(III) \quad K_i = \tilde{K}_i; \quad i = \overline{1, n-3}, \quad \text{if } n \geq 4.$$

Since the distance between corresponding points is the constant  $r$ , we have

$$(2.2) \quad \tilde{\mathbf{c}} = \mathbf{c} + r \mathbf{f}_1.$$

Using  $F = AE$  we have

$$\mathbf{f}_1 = \sum_{j=1}^{n-1} a_{1j} \mathbf{e}_j,$$

which implies

$$\tilde{\mathbf{c}} = \mathbf{c} + r \sum_{j=1}^{n-1} a_{1j} \mathbf{e}_j.$$

We have already seen that the first  $n-2$  rows of  $A\tilde{E}$  coincide with the first  $n-2$  columns of  $AE$ . Thus

$$(2.3) \quad \langle \mathbf{f}_1, \tilde{\mathbf{e}}_1 \rangle = \langle \mathbf{f}_1, \mathbf{e}_1 \rangle = a_{11}.$$

Differentiating  $(\tilde{\mathbf{c}} - \mathbf{c})^2 = r^2$  we obtain  $2\langle \tilde{\mathbf{c}} - \mathbf{c}, \dot{\tilde{\mathbf{c}}}|\tilde{\mathbf{e}}_1 - \mathbf{e}_1 \rangle = 0$ , which by (2.2) and (2.3) becomes  $|\dot{\tilde{\mathbf{c}}}| = 1$ , hence  $\tilde{\mathbf{c}}$  is also of unit speed. Differentiating (2.3) and using the Frenét formulae for  $\mathbf{e}_j$  we obtain

$$\begin{aligned} \tilde{\mathbf{e}}_1 = & (1 + ra_{11} - rK_1a_{12})\mathbf{e}_1 + r \sum_{j=2}^{n-2} (a_{1j} - K_j a_{1,j+1} + K_{j-1} a_{1,j-1})\mathbf{e}_j \\ & + r(a_{1,n-1} + a_{1,n-2}K_{n-2})\mathbf{e}_{n-1} + ra_{1,n-1}K_{n-1}\mathbf{e}_n. \end{aligned}$$

Comparing this with (2.1) and using  $a_{1,n-1} = -a_{n-1,1}$ , we obtain

$$(IV) \quad \left\{ \begin{array}{l} K_1 = \frac{ra_{11} + a_{n-1,1}^2(1 - \cos \theta)}{ra_{12}}, \\ K_j = \frac{a_{1j} + a_{n-1,1}a_{n-1,j}(1 - \cos \theta) + K_{j-1}a_{1,j-1}}{a_{1,j+1}}; \\ \quad j = \overline{2, n-2}, \\ K_{n-1} = \frac{\sin \theta}{r}. \end{array} \right.$$

In conclusion, (III) and (IV)<sub>3</sub> are exactly the assertions of our theorem.

For  $n > 4$  if we fix a unit speed curve  $\mathbf{c}$  in  $\mathbf{R}^n$  with a given constant torsion, the system (0) + (I) + (II) + (IV) is underdetermined.

But this system is equivalent to the conditions (1), (2), (3) of Theorem 3.1. In conclusion, for every curve  $\mathbf{c} \subset \mathbf{R}^n$ ;  $n > 4$  with  $K_{n-1} = a$ , where  $a$  is a given constant, and every vector  $\mathbf{v} \in T_{\mathbf{c}(0)}\mathbf{R}^n$ , we can find an infinite number of curves  $\tilde{\mathbf{c}} \subset \mathbf{R}^n$  satisfying the conditions (1), (2), (3) of Theorem 3.1 and such that  $\sin \theta = ar$  and  $\tilde{\mathbf{c}}(0) - \mathbf{c}(0) = \mathbf{v}$ , where  $T_{\mathbf{c}(0)}\mathbf{R}^n$  is the tangent space of  $\mathbf{R}^n$  in  $\mathbf{c}(0)$ .

*Remark 2.2.* The case  $n = 4$  is a special one, since for this dimension the condition (I) implies that the matrix  $A$  must be of the form

$$A = \begin{bmatrix} 0 & \cos \beta & -\sin \beta & 0 \\ 0 & \sin \beta & \cos \beta & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix},$$

hence the discussion of this case reduces to the 3-dimensional one.

*Example 2.3.* The following example will be given for  $n = 5$ . Let  $r > 0$ ,  $a, b, c, \theta$ , be five constants, such that

$$4(a^2 + b^2) \sin^4 \frac{\theta}{2} = c^2 r^2.$$

Consider the curve  $\mathbf{c} : s \mapsto \exp(s\Omega)$ , where

$$\Omega = \begin{bmatrix} 0 & a & 0 & 0 & 0 \\ -a & 0 & b & 0 & 0 \\ 0 & -b & 0 & c & 0 \\ 0 & 0 & -c & 0 & \frac{\sin \theta}{r} \\ 0 & 0 & 0 & -\frac{\sin \theta}{r} & 0 \end{bmatrix}.$$

By the Frenét formulae, the curvatures of  $\mathbf{c}$  are  $K_1 = a$ ,  $K_2 = b$ ,  $K_3 = c$ ,  $K_4 = r^{-1} \sin \theta$ . Integrating the system (0) + (I) + (II) + (IV), we obtain

$$\begin{aligned} \tilde{\mathbf{c}}(s) = & c(s) - \left[ \frac{4}{r^3} \frac{b^2}{a^2} \sin^6 \frac{\theta}{2} s - a\alpha(s) \right] e_1 \\ & + \dot{\alpha}(s)e_2 + \left[ \left( \frac{2}{r} \frac{b}{a} \sin^2 \frac{\theta}{2} - \frac{4}{r^2} \sin^6 \frac{\theta}{2} \right) s - b\alpha(s) \right] e_3 + \frac{2}{r} \frac{b}{ac} \sin^2 \frac{\theta}{2} e_4, \end{aligned}$$

and

$$a_{43} = -\frac{2}{r} \frac{1}{c} \sin^2 \frac{\theta}{2},$$

where  $\alpha$  satisfies the following differential equation:

$$\begin{aligned} & \dot{\alpha}^2(s) + \left[ \frac{4}{r^3} \frac{b^2}{a^2} \sin^6 \frac{\theta}{2} s - a\alpha(s) \right]^2 \\ & + \left[ \left( \frac{1}{r} \frac{2b}{a} \sin^2 \frac{\theta}{2} - \frac{4}{r^2} \sin^6 \frac{\theta}{2} \right) s - b\alpha(s) \right]^2 + \frac{1}{r^2} \frac{4b^2}{a^2 c^2} \sin^4 \frac{\theta}{2} = 1 \end{aligned}$$

In particular the constant solutions of this equation can be found explicitly by solving a quadratic polynomial equation.

Using the formulae  $\tilde{K}_1 = K_1, \dots, \tilde{K}_{n-3} = K_{n-3}, \tilde{K}_{n-1} = K_{n-2}$  and  $\tilde{K}_{n-2} = K_{n-2} + 2K_{n-1} \tan \frac{\theta}{2} a_{n-1, n-2}$ , we obtain

$$\tilde{K}_1 = a, \quad \tilde{K}_2 = b, \quad \tilde{K}_4 = \frac{\sin \theta}{r},$$



and

$$\tilde{K}_3 = c - \frac{8}{r^2} \frac{1}{c} \sin^4 \frac{\theta}{2},$$

respectively.

Hence, if we impose the initial conditions  $\tilde{E}(0) = I$ , where  $I$  is the identical matrix, the Frenét formulae of  $\tilde{\mathbf{c}}$  yields

$$\tilde{\mathbf{c}}(s) = \exp s \tilde{\Omega},$$

where

$$\tilde{\Omega} = \begin{bmatrix} 0 & a & 0 & 0 & 0 \\ -a & 0 & b & 0 & 0 \\ 0 & -b & 0 & c - \frac{1}{c} \frac{8}{r^2} \sin^4 \frac{\theta}{2} & 0 \\ 0 & 0 & -c + \frac{1}{c} \frac{8}{r^2} \sin^4 \frac{\theta}{2} & 0 & \frac{\sin \theta}{r} \\ 0 & 0 & 0 & -\frac{\sin \theta}{r} & 0 \end{bmatrix}.$$

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